

02. Thermodynamic Entropy S_{TD}

1. Clausius' Inequality

1854. "On a modified form of the second fundamental theorem in the mechanical theory of heat".

1865. "On several convenient forms of the fundamental equations of the mechanical theory of heat."

- Clausius' "Fundamental Principle" (1854):



"Heat can never pass from a colder to a warmer body *without some other change, connected therewith*, occurring at the same time."

Now formulate this "algebraically"...

1. Clausius' Inequality
2. Thermodynamic Entropy S_{TD}
3. Principle of Increasing S_{TD}
4. S_{TD} and the Approach to Equilibrium
5. Summary of 2nd Law

- Consider a cyclic process involving infinitesimal transfers of heat $\delta Q/T$ between a system and a reservoir at lower temperature:

- Let $+\delta Q/T$ represent an emission of heat by the system to the reservoir.
- Let $-\delta Q/T$ represent an absorption of heat by the system from the reservoir.

system

$$+\frac{\delta Q}{T} \downarrow \quad \uparrow -\frac{\delta Q}{T}$$

reservoir



"The algebraic sum of all the transformations which occur in a cyclical process can only be positive." (1854)

Or: $\oint \frac{\delta Q}{T} \geq 0$

Why? If the sum were negative, then the overall effect would be a passage of heat from lower to higher temp.

Moreover: If the process is reversible, then the sum is zero.

- It can't be negative.
- If it were positive, the process could be reversed to produce a negative result.

- 1865: Change of sign convention:

- Let $+\delta Q/T$ represent absorption of heat by the system.
- Let $-\delta Q/T$ represent emission of heat by the system.

$$\oint \frac{\delta Q}{T} \leq 0$$

Clausius' Inequality

- For reversible processes, let $dS_{\text{TD}} = \delta Q_R/T$. Call S_{TD} "thermodynamic entropy".

"... I propose to call the magnitude [S_{TD}] the [thermodynamic] *entropy* of the body... I have intentionally formed the word *entropy* so as to be as similar as possible to the word *energy*; for the two magnitudes to be denoted by these words are so nearly allied in their physical meanings, that a certain similarity in designation appears to be desirable." (1865)



- For a thermally isolated system, can show that the 2nd Law entails:
$$\int_{\sigma_1}^{\sigma_2} dS_{\text{TD}} = S_{\text{TD}}(\sigma_2) - S_{\text{TD}}(\sigma_1) \geq 0$$

What this means: For a thermally isolated system undergoing an energy transformation, the thermodynamic entropy of the final equilibrium state σ_2 cannot be less than the entropy of the initial equilibrium state σ_1 .



"... [W]e may express in the following manner the fundamental laws of the universe which correspond to the two fundamental theorems of the mechanical theory of heat:

1. *The energy of the universe is constant.*

2. *The [thermodynamic] entropy of the universe tends to a maximum.*"

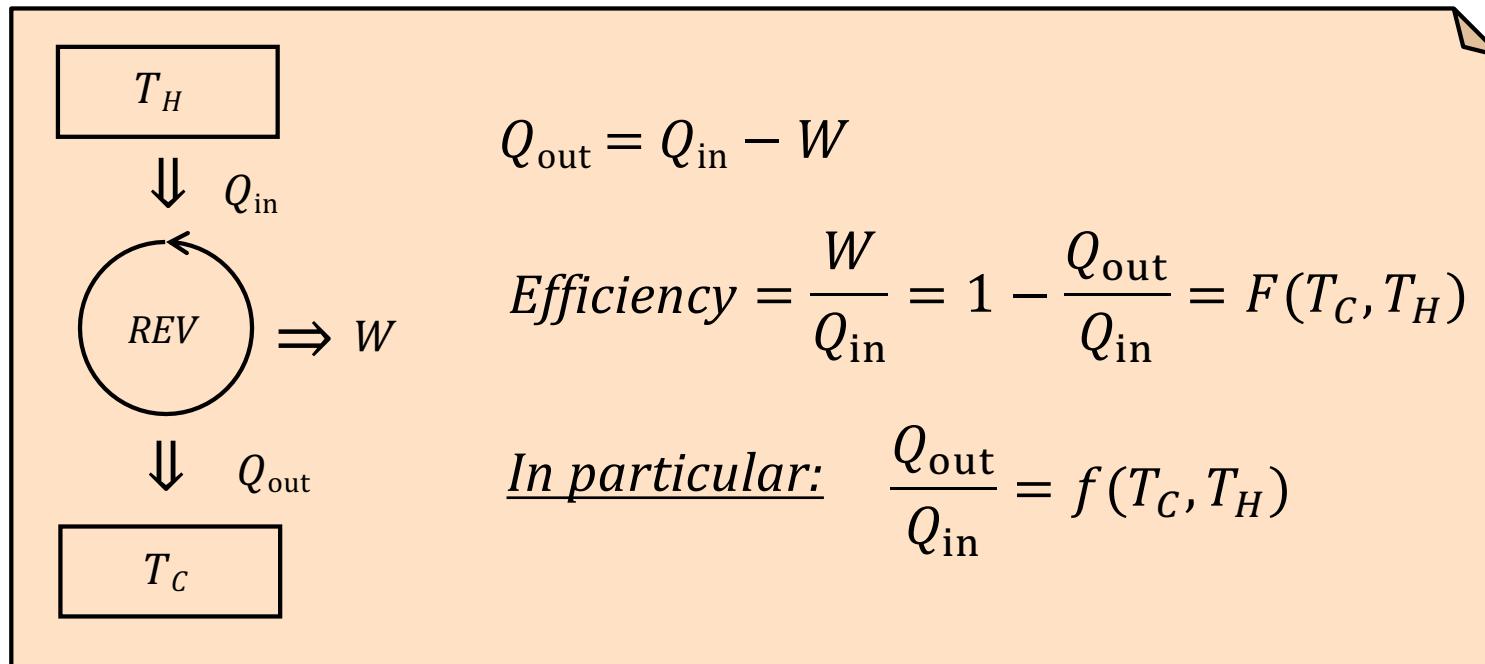
Aside: Contemporary Derivation of Clausius' inequality

- First: Let's derive the important relation for reversible heat engines

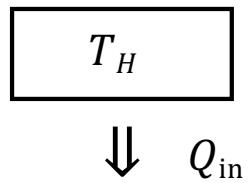
$$\frac{Q_{\text{out}}}{Q_{\text{in}}} = \frac{T_C}{T_H}$$

where the temperature is measured by the absolute Kelvin scale.

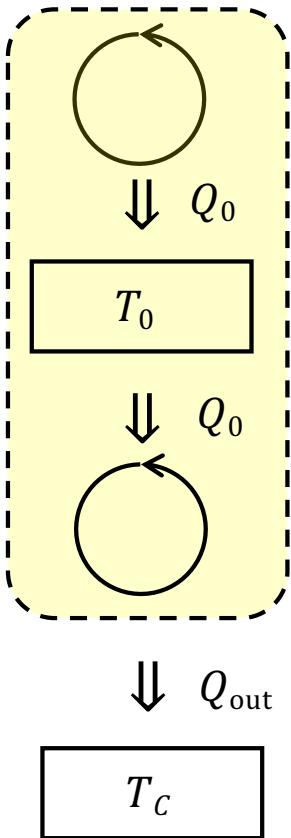
- Recall (Carnot's Claim #2): The efficiency of a reversible heat engine is a function *only* of the temperatures of the hot and cold places.



- Consider a multi-stage *reversible* heat engine:



- Note: $\frac{Q_{\text{out}}}{Q_{\text{in}}} = \frac{Q_{\text{out}}}{Q_0} \frac{Q_0}{Q_{\text{in}}}$



- So: $\frac{Q_{\text{out}}}{Q_{\text{in}}} = f(T_C, T_H) = f(T_C, T_0) \left(\frac{1}{f(T_H, T_0)} \right) = \frac{f(T_C)}{f(T_H)}$
- Now choose: $f(T_C) = T_C$, $f(T_H) = T_H$ Thomson's (1848)
"absolute" temp scale.
- For this "Kelvin" temp scale, and for reversible heat engines:

$$\frac{Q_{\text{out}}}{Q_{\text{in}}} = \frac{T_C}{T_H}$$

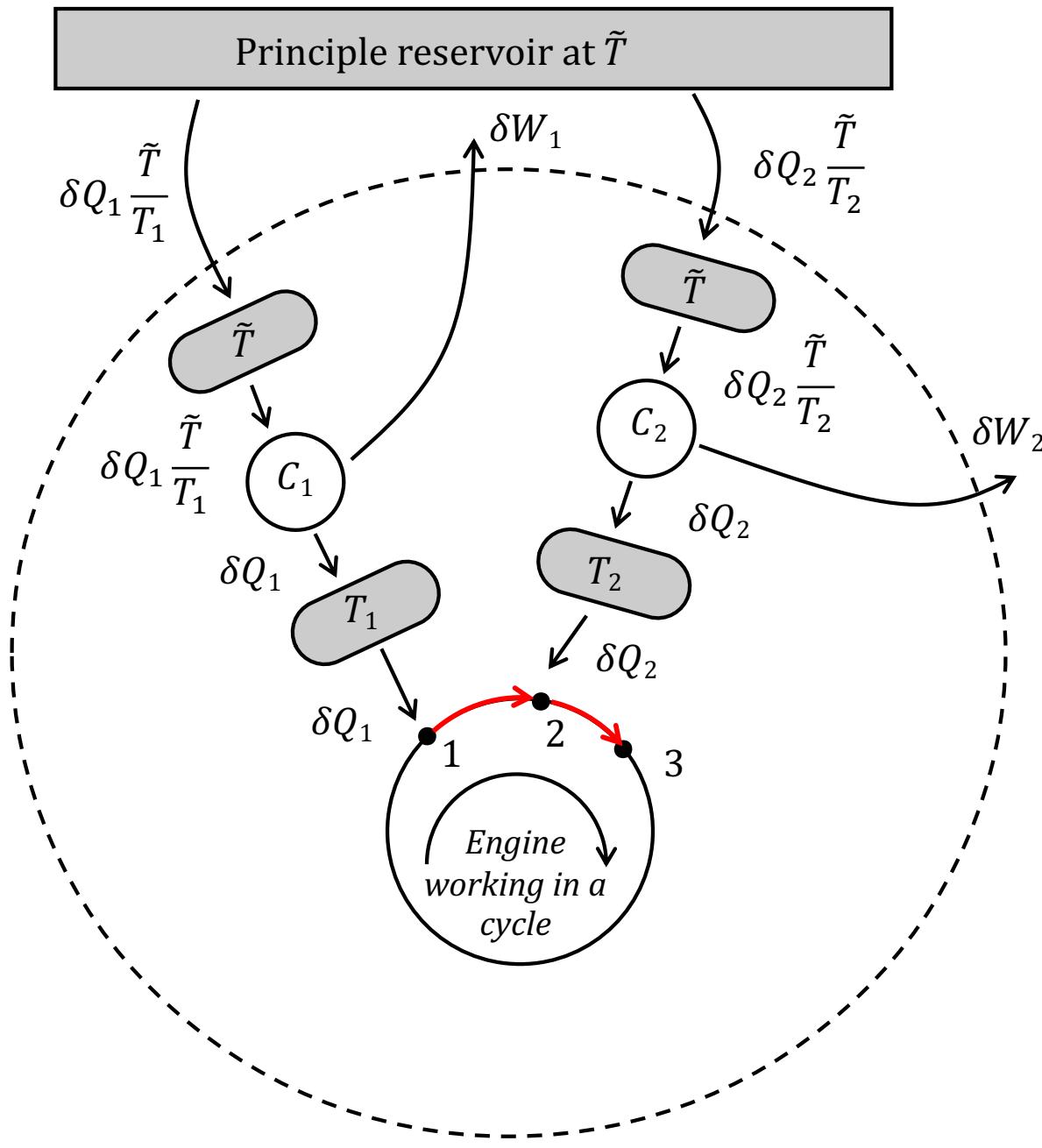
or

$$Q_{\text{in}} = Q_{\text{out}} \frac{T_H}{T_C}$$

Now: Let's derive Clausius' Inequality...

- Consider the following engine working in a cycle in which the initial and final states are identical.

$$Q_{\text{in}} = Q_{\text{out}} \frac{T_H}{T_C}$$

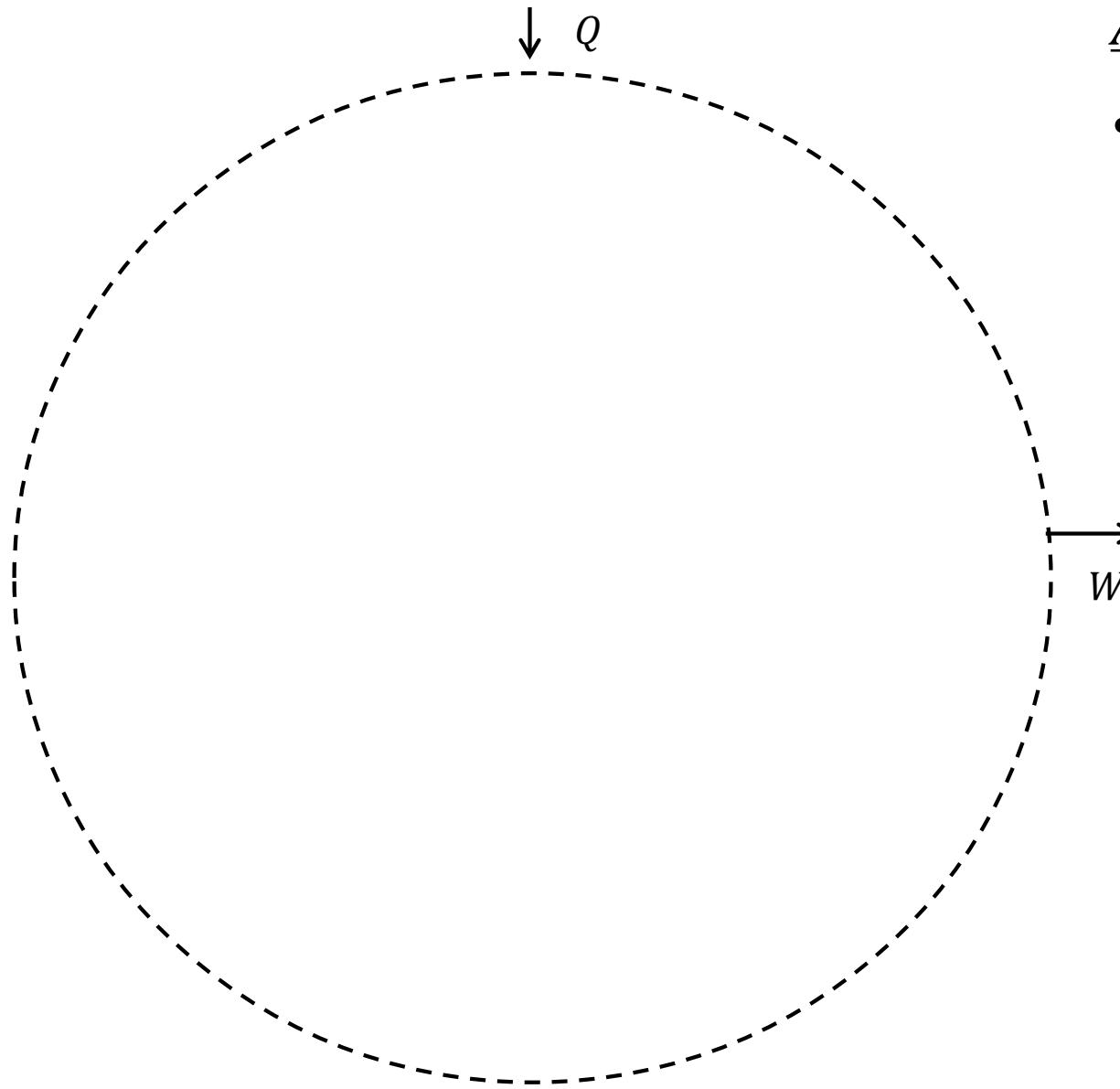


- Initial state 1 of working substance at temp T_1 .
- Use reservoir at T_1 to inject heat δQ_1 to move to state 2 at temp T_2 .
- Resupply T_1 using reversible heat engine C_1 , which takes heat $\delta Q_1(\tilde{T}/T_1)$ from reservoir at \tilde{T} , and performs work δW_1 .
- Resupply reservoir at \tilde{T} with heat $\delta Q_1(\tilde{T}/T_1)$ from principle reservoir.
- Repeat process.

- Consider the following engine working in a cycle in which the initial and final states are identical.

Principle reservoir at \tilde{T}

$\downarrow Q$



After complete cycle:

- Total heat supplied is

$$Q = \sum_i \delta Q_i \frac{\tilde{T}}{T_i}$$

- Total work output is

$$W = \sum_i \delta W_i$$

- $\Delta U = U_f - U_i = 0$

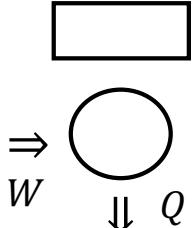
for a cycle

- So: $0 = -W + Q$

- Or: $Q = W$

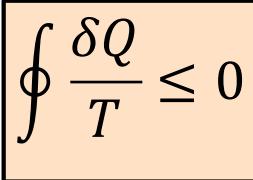
But! This is a violation of the 2nd Law (Thomson version)!

- So:
 - Either W and Q must be negative,  *work is done to the system and an equal amount of heat is extracted from it*
 - Or W and Q must be zero.



- Thus: $W = Q \leq 0$, or $\tilde{T} \sum_i \frac{\delta Q_i}{T_i} \leq 0$ or $\sum_i \frac{\delta Q_i}{T_i} \leq 0$



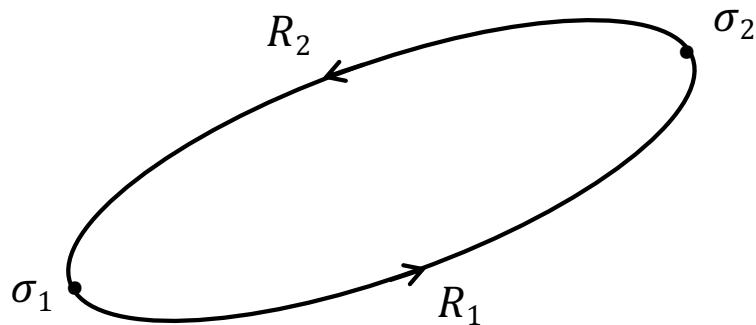
- Hence:  *Clausius' Inequality*

- What if the cycle is reversible?

- Then: $-\oint \frac{\delta Q_R}{T} \leq 0$ or $\oint \frac{\delta Q_R}{T} \geq 0$
- So: In order to be consistent with the first result, $\oint \frac{\delta Q_R}{T} = 0$.

2. Thermodynamic Entropy S_{TD}

- Consider a *reversible* cycle:



- Start in initial equilibrium state σ_1 .
- Take reversible path R_1 to equilibrium state σ_2 .
- Return to σ_1 via reversible path R_2 .

- Clausius' inequality is $\oint \frac{\delta Q_R}{T} = \int_{R_1}^{\sigma_2} \frac{\delta Q_R}{T} + \int_{R_2}^{\sigma_1} \frac{\delta Q_R}{T} = 0$

- Thus: $\int_{R_1}^{\sigma_2} \frac{\delta Q_R}{T} = - \int_{R_2}^{\sigma_1} \frac{\delta Q_R}{T} = \int_{R_2}^{\sigma_2} \frac{\delta Q_R}{T}$

- So: $\int_{\sigma_1}^{\sigma_2} \frac{\delta Q_R}{T}$ is *path-independent!*

- Which means: It can be represented by a path-independent function, call it S_{TD} :

$$\Delta S_{\text{TD}} = S_{\text{TD}}(\sigma_2) - S_{\text{TD}}(\sigma_1) \equiv \int_{\sigma_1}^{\sigma_2} \frac{\delta Q_R}{T}$$

"thermodynamic entropy"

Def. 1 (Thermodynamic entropy). The **thermodynamic entropy** $S_{\text{TD}}(\sigma_2)$ of an equilibrium state σ_2 is the ratio of the change in heat to temperature of a *reversible* process that connects an initial equilibrium state σ_1 to σ_2 :

$$S_{\text{TD}}(\sigma_2) \equiv \int_{\sigma_1}^{\sigma_2} \frac{\delta Q_R}{T} + S_0$$

arbitrary constant

Characteristics

1. Only defined for *reversible processes*; *i.e.*, processes that are "quasi-static".
 - *Quasi-static process* = succession of equilibrium states.
 - *Equilibrium state* = state of system in which macroscopic properties (*i.e.*, temp, volume, pressure, *etc.*) are constant.
2. Only defined for *equilibrium states*.
3. For infinitesimal changes in S_{TD} , can write

$$dS_{\text{TD}} = \delta Q_R/T$$

1/T is an 'integrating factor' that converts a path-dependent function Q into a path-independent function S_{TD}

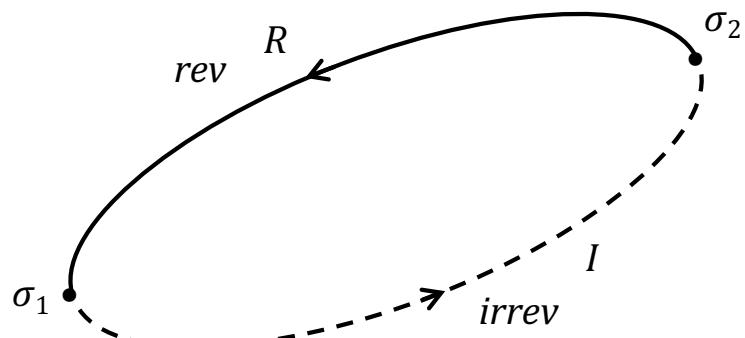
For an *irreversible* process connecting equilibrium states σ_1 and σ_2 , S_{TD} can still be calculated if there is, in principle, a reversible process that connects σ_1 and σ_2 .

Ex: Heating a beaker of water.

- *No reference to "disorder" or "chaos"!*
- *No reference to molecules or particles (gas or otherwise)!*
- *No reference to "information"!*

3. Principle of Increasing S_{TD}

Consider an *irreversible* cycle:



Irreversible cycle consisting of an irreversible process I from σ_1 to σ_2 , followed by a reversible process R from σ_2 back to σ_1 .

- Clausius' inequality is
$$I \int_{\sigma_1}^{\sigma_2} \frac{\delta Q}{T} + R \int_{\sigma_2}^{\sigma_1} \frac{\delta Q_R}{T} < 0 \quad \text{or} \quad I \int_{\sigma_1}^{\sigma_2} \frac{\delta Q}{T} - R \int_{\sigma_1}^{\sigma_2} \frac{\delta Q_R}{T} < 0$$
- Thus:
$$\Delta S_{TD} = R \int_{\sigma_1}^{\sigma_2} \frac{\delta Q_R}{T} > I \int_{\sigma_1}^{\sigma_2} \frac{\delta Q}{T}$$
 Note: If the cycle was reversible (i.e., if the path I was reversible), then $>$ would become $=$.
- So in general:
$$\Delta S_{TD} = R \int_{\sigma_1}^{\sigma_2} \frac{\delta Q_R}{T} \geq I \int_{\sigma_1}^{\sigma_2} \frac{\delta Q}{T}$$
- Now: Suppose the path from σ_1 to σ_2 is *thermally isolated*; i.e., $\delta Q = 0$.
- Then:
$$\Delta S_{TD} \geq 0 \quad \text{or} \quad S_{TD}(\sigma_2) \geq S_{TD}(\sigma_1)$$

The change in thermodynamic entropy for a thermally isolated irreversible process between equilibrium states increases, and is unaltered for a reversible process.

4. S_{TD} and the Approach to Equilibrium

- How does the Principle of Increasing S_{TD} relate to the Equilibrium Principle?

One way of formulating the 2nd Law!

The Minus 1st Law!

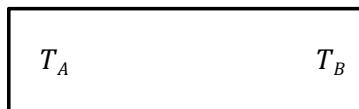
- The "approach to equilibrium" is a process that connects a *non-equilibrium* state with an equilibrium state!

How is S_{TD} defined for such a process? And does it increase/remain unaltered?

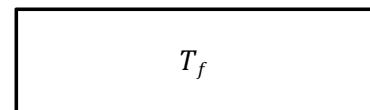
General method:

- System in initial *non-equilibrium* state can be decomposed into subsystems, each in an initial *equilibrium* state.
- Process that takes system from initial non-equilibrium state to final equilibrium state can be decomposed into a sum of processes that take each subsystem from its initial equilibrium state to final equilibrium state.
- Each sub-process has well-defined change in S_{TD} , and sum of these (i.e., change in S_{TD} for entire system) cannot be negative!

$T_A > T_B$
initial non-equilibrium state

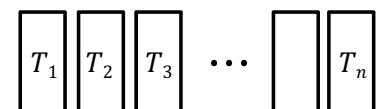


$$\Delta S_{TD} = \Delta S_{TD}^1 + \dots + \Delta S_{TD}^n$$

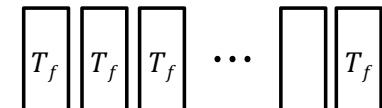


final equilibrium state

$T_1 = T_A < T_2 < \dots < T_n = T_B$
initial equilibrium states



$$\Delta S_{TD}^1 \quad \dots \quad \Delta S_{TD}^n$$

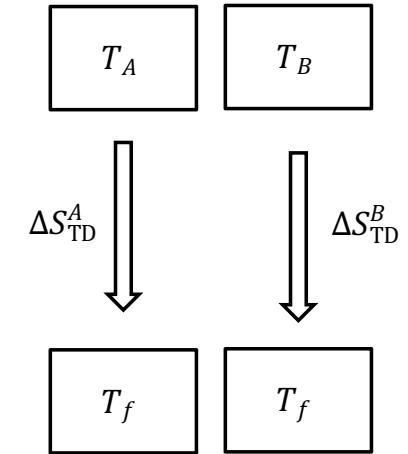


final equilibrium states

Ex. System composed of subsystems A, B with initial temps T_A, T_B and heat capacities $C_A \equiv \delta Q_A/dT, C_B \equiv \delta Q_B/dT$ that are brought into contact and then allowed to reach equilibrium at temp T_f .

- System: initial *non-equilibrium* state σ_i , final *equilibrium* state σ_f .
- A, B : initial *equilibrium* states σ_i^A, σ_i^B , final *equilibrium* states σ_f^A, σ_f^B .
- Suppose σ_i^A, σ_f^A are connected by a reversible process, at each step of which A absorbs a small amount of heat $\delta Q_A = C_A dT$ from a reservoir resulting in an increase dT in temperature.
- Change in S_{TD} for A is:

$$\Delta S_{\text{TD}}^A = S_{\text{TD}}^A(\sigma_f^A) - S_{\text{TD}}^A(\sigma_i^A) = \int_{\sigma_i^A}^{\sigma_f^A} \frac{\delta Q_A}{T} = \int_{T_A}^{T_f} \frac{C_A dT}{T} = C_A \ln \frac{T_f}{T_A}$$



Similarly for ΔS_{TD}^B

- Change in S_{TD} for entire system is:

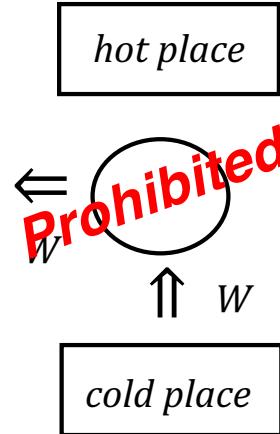
$$\Delta S_{\text{TD}}^A + \Delta S_{\text{TD}}^B = C_A \ln \frac{T_f}{T_A} + C_B \ln \frac{T_f}{T_B} \quad \text{Claim: This expression cannot be negative!}$$

$$\begin{aligned} C_A \ln \frac{T_f}{T_A} + C_B \ln \frac{T_f}{T_B} &\geq C_A(1 - T_A/T_f) + C_B(1 - T_B/T_f) \quad \text{ln}y \geq 1 - 1/y \\ &= T_f^{-1}[C_A(T_f - T_A) + C_B(T_f - T_B)] \\ &= T_f^{-1}(Q_A + Q_B) \\ &= 0 \end{aligned}$$

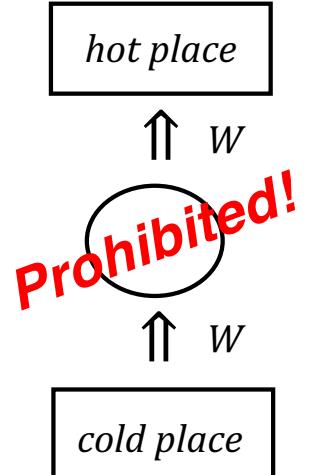
total work = 0

5. Summary of 2nd Law of Thermodynamics

(1) Clausius Form: No cyclic process in which heat is transferred from cold to hot place without work input:



(2) Thomson Form: No cyclic process in which there is a conversion of heat to work without exhaust:



Consequence of 2nd Law:

The *thermodynamic entropy* S_{TD} of a thermally isolated irreversible process between equilibrium states increases, and is unaltered for a reversible process.

Absolute statements!

Meant to hold for any system subject to thermodynamical analysis.

Summary of Entailments

