

## 02. Thermodynamic Entropy $S_{TD}$

1. Clausius' Inequality
2. Thermodynamic Entropy  $S_{TD}$
3. Principle of Increasing  $S_{TD}$
4.  $S_{TD}$  and the Approach to Equilibrium
5. Summary of 2nd Law

### 1. Clausius' Inequality

1854. "On a modified form of the second fundamental theorem in the mechanical theory of heat".

1865. "On several convenient forms of the fundamental equations of the mechanical theory of heat."

- Clausius' "Fundamental Principle" (1854):

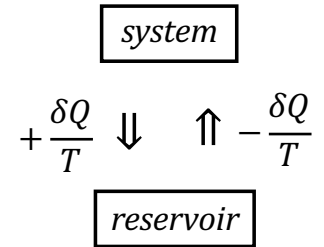


"Heat can never pass from a colder to a warmer body *without some other change, connected therewith, occurring at the same time.*"

*Now formulate this "algebraically"...*

- Consider a cyclic process involving infinitesimal transfers of heat  $\delta Q/T$  between a system and a reservoir at lower temperature:

- Let  $+\delta Q/T$  represent an emission of heat by the system to the reservoir.
- Let  $-\delta Q/T$  represent an absorption of heat by the system from the reservoir.



"The algebraic sum of all the transformations which occur in a cyclical process can only be positive." (1854)

Or:  $\oint \frac{\delta Q}{T} \geq 0$

Why? If the sum were negative, then the overall effect would be a passage of heat from lower to higher temp.

Moreover: If the process is reversible, then the sum is zero.

- It can't be negative.
- If it were positive, the process could be reversed to produce a negative result.

- 1865: Change of sign convention:

- Let  $+\delta Q/T$  represent absorption of heat by the system.
- Let  $-\delta Q/T$  represent emission of heat by the system.

$$\oint \frac{\delta Q}{T} \leq 0$$

Clausius' Inequality

- For reversible processes, let  $dS_{\text{TD}} = \delta Q_R/T$ . Call  $S_{\text{TD}}$  "thermodynamic entropy".

"... I propose to call the magnitude [ $S_{\text{TD}}$ ] the [thermodynamic] *entropy* of the body... I have intentionally formed the word *entropy* so as to be as similar as possible to the word *energy*; for the two magnitudes to be denoted by these words are so nearly allied in their physical meanings, that a certain similarity in designation appears to be desirable." (1865)



- For a thermally isolated system, can show that the 2nd Law entails: 
$$\int_{\sigma_1}^{\sigma_2} dS_{\text{TD}} = S_{\text{TD}}(\sigma_2) - S_{\text{TD}}(\sigma_1) \geq 0$$

*What this means:* For a thermally isolated system undergoing an energy transformation, the thermodynamic entropy of the final equilibrium state  $\sigma_2$  cannot be less than the entropy of the initial equilibrium state  $\sigma_1$ .



"... [W]e may express in the following manner the fundamental laws of the universe which correspond to the two fundamental theorems of the mechanical theory of heat:

1. *The energy of the universe is constant.*
2. *The [thermodynamic] entropy of the universe tends to a maximum."*

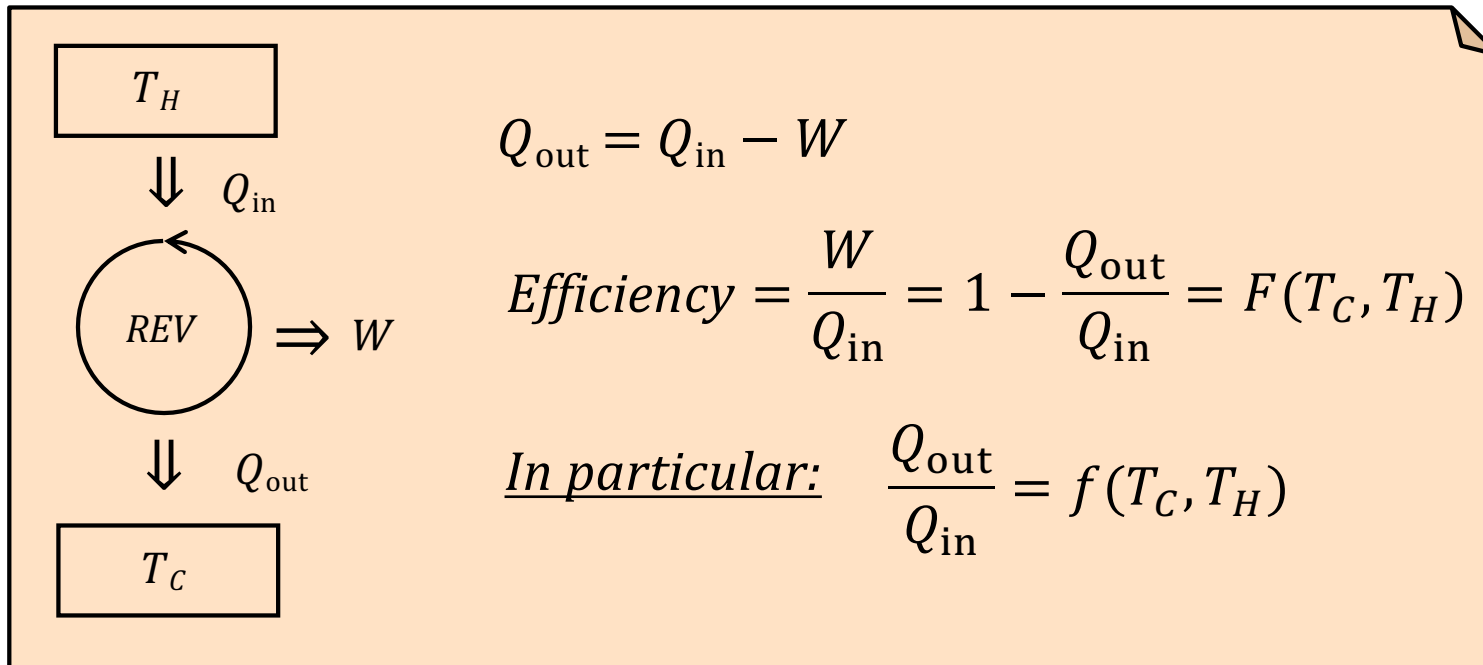
### Aside: Contemporary Derivation of Clausius' inequality

- First: Let's derive the important relation for reversible heat engines

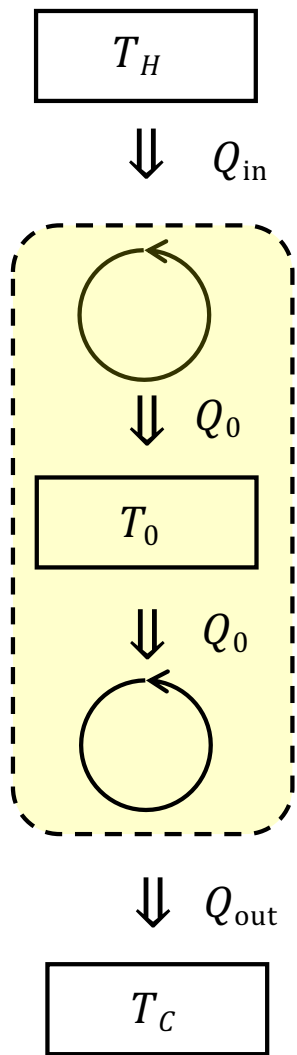
$$\frac{Q_{\text{out}}}{Q_{\text{in}}} = \frac{T_C}{T_H}$$

where the temperature is measured by the absolute Kelvin scale.

- Recall (Carnot's Claim #2): The efficiency of a reversible heat engine is a function *only* of the temperatures of the hot and cold places.



- Consider a multi-stage *reversible* heat engine:



- Note:  $\frac{Q_{\text{out}}}{Q_{\text{in}}} = \frac{Q_{\text{out}}}{Q_0} \frac{Q_0}{Q_{\text{in}}}$

- So:  $\frac{Q_{\text{out}}}{Q_{\text{in}}} = f(T_C, T_H) = f(T_C, T_0) \left( \frac{1}{f(T_H, T_0)} \right) = \frac{f(T_C)}{f(T_H)}$

- Now choose:  $f(T_C) = T_C$ ,  $f(T_H) = T_H$  ← Thomson's (1848) "absolute" temp scale.

- For this "Kelvin" temp scale, and for reversible heat engines:

$$\frac{Q_{\text{out}}}{Q_{\text{in}}} = \frac{T_C}{T_H}$$

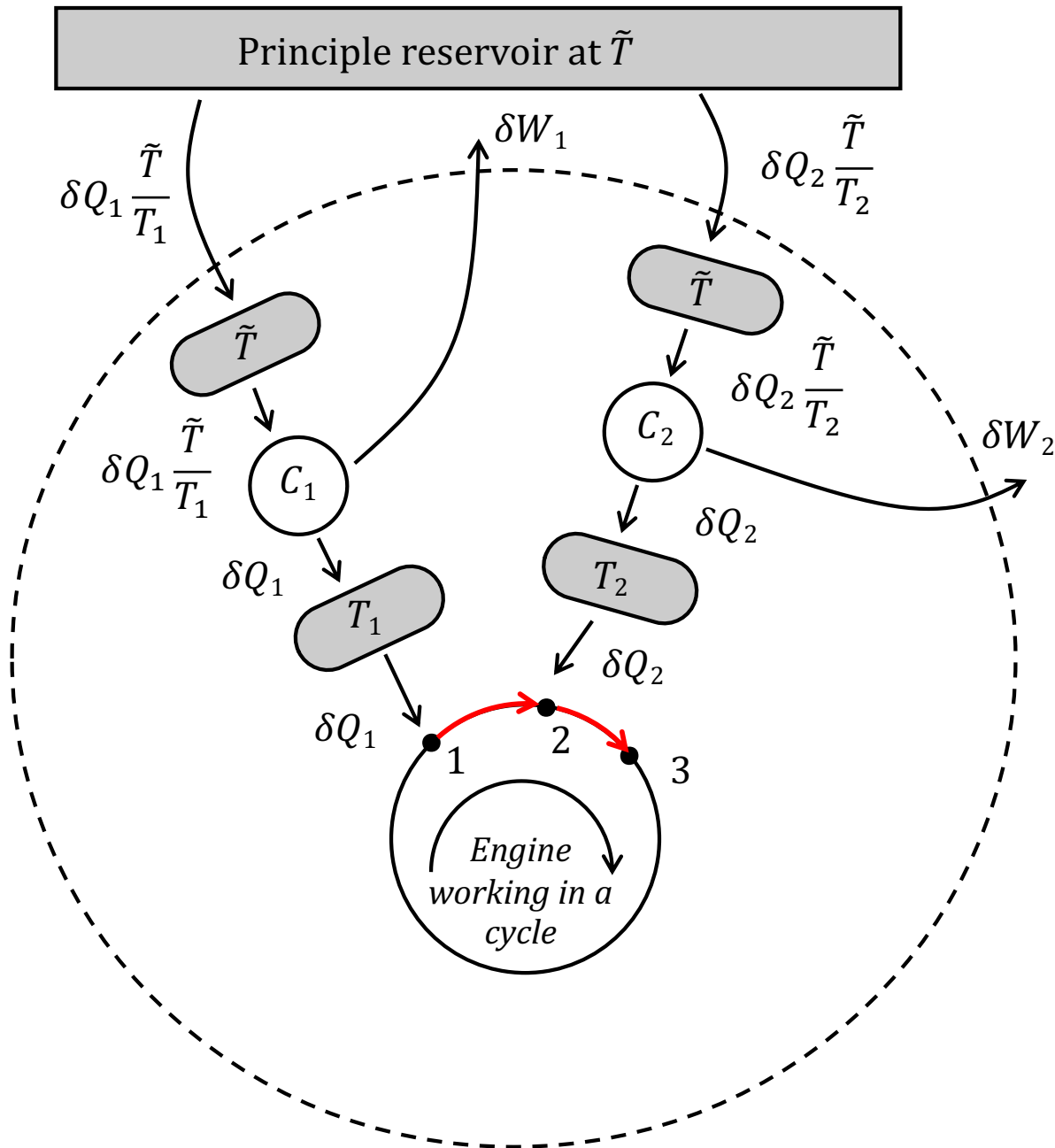
or

$$Q_{\text{in}} = Q_{\text{out}} \frac{T_H}{T_C}$$

Now: Let's derive Clausius' Inequality...

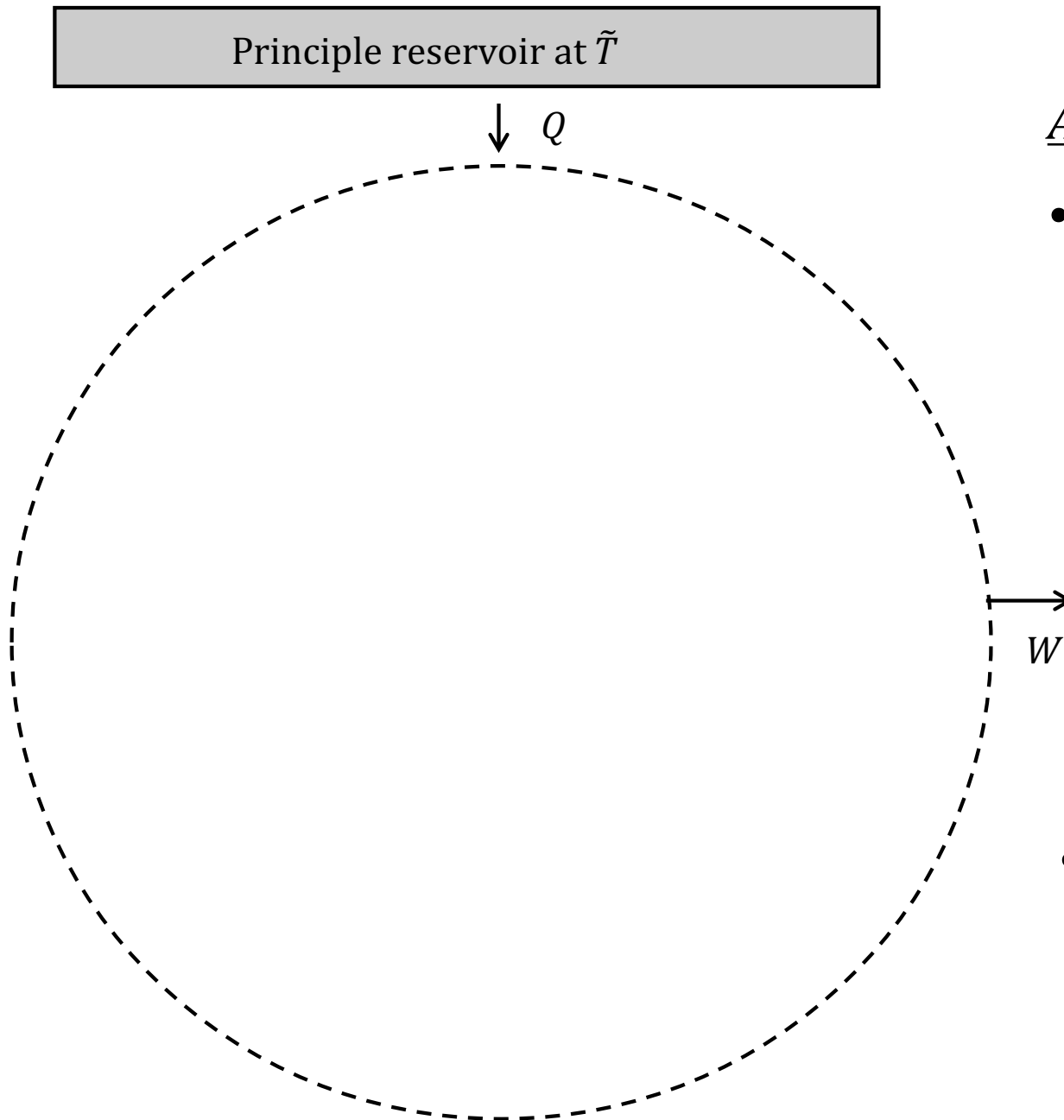
- Consider the following engine working in a cycle in which the initial and final states are identical.

$$Q_{\text{in}} = Q_{\text{out}} \frac{T_H}{T_C}$$



- Initial state 1 of working substance at temp  $T_1$ .
- Use reservoir at  $T_1$  to inject heat  $\delta Q_1$  to move to state 2 at temp  $T_2$ .
- Resupply  $T_1$  using reversible heat engine  $C_1$ , which takes heat  $\delta Q_1(\tilde{T}/T_1)$  from reservoir at  $\tilde{T}$ , and performs work  $\delta W_1$ .
- Resupply reservoir at  $\tilde{T}$  with heat  $\delta Q_2(\tilde{T}/T_2)$  from principle reservoir.
- Repeat process.

- Consider the following engine working in a cycle in which the initial and final states are identical.



After complete cycle:

- Total heat supplied is

$$Q = \sum_i \delta Q_i \frac{\tilde{T}}{T_i}$$

- Total work output is

$$W = \sum_i \delta W_i$$


- $\Delta U = U_f - U_i = 0$

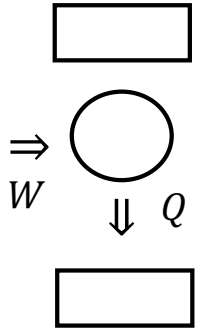
*for a cycle*

- So:  $0 = -W + Q$

- Or:  $Q = W$

*But! This is a violation of the 2nd Law (Thomson version)!*

- So:
  - Either  $W$  and  $Q$  must be negative,  *work is done to the system and an equal amount of heat is extracted from it*
  - Or  $W$  and  $Q$  must be zero.



- Thus:  $W = Q \leq 0$ , or  $\tilde{T} \sum_i \frac{\delta Q_i}{T_i} \leq 0$  or  $\sum_i \frac{\delta Q_i}{T_i} \leq 0$

- Hence:  $\oint \frac{\delta Q}{T} \leq 0$  *Clausius' Inequality*

- What if the cycle is reversible?

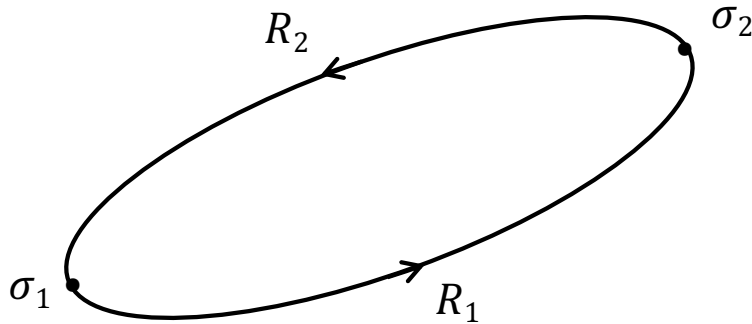
- Then:  $-\oint \frac{\delta Q_R}{T} \leq 0$  or  $\oint \frac{\delta Q_R}{T} \geq 0$

- So: In order to be consistent with the first result,  $\oint \frac{\delta Q_R}{T} = 0$ .



## 2. Thermodynamic Entropy $S_{\text{TD}}$

- Consider a *reversible* cycle:



- Start in initial equilibrium state  $\sigma_1$ .
- Take reversible path  $R_1$  to equilibrium state  $\sigma_2$ .
- Return to  $\sigma_1$  via reversible path  $R_2$ .

- Clausius' inequality is 
$$\oint \frac{\delta Q_R}{T} = \int_{R_1}^{\sigma_2} \frac{\delta Q_R}{T} + \int_{R_2}^{\sigma_1} \frac{\delta Q_R}{T} = 0$$

- Thus: 
$$\int_{R_1}^{\sigma_2} \frac{\delta Q_R}{T} = - \int_{R_2}^{\sigma_2} \frac{\delta Q_R}{T} = \int_{R_2}^{\sigma_1} \frac{\delta Q_R}{T}$$

- So:  $\int_{\sigma_1}^{\sigma_2} \frac{\delta Q_R}{T}$  is *path-independent*!

- Which means: It can be represented by a path-independent function, call it  $S_{\text{TD}}$ :

$$\Delta S_{\text{TD}} = S_{\text{TD}}(\sigma_2) - S_{\text{TD}}(\sigma_1) \equiv \int_{\sigma_1}^{\sigma_2} \frac{\delta Q_R}{T}$$

*"thermodynamic  
entropy"*

**Def. 1** (*Thermodynamic entropy*). The **thermodynamic entropy**  $S_{\text{TD}}(\sigma_2)$  of an equilibrium state  $\sigma_2$  is the ratio of the change in heat to temperature of a *reversible* process that connects an initial equilibrium state  $\sigma_1$  to  $\sigma_2$ :

$$S_{\text{TD}}(\sigma_2) \equiv \int_{\sigma_1}^{\sigma_2} \frac{\delta Q_R}{T} + S_0 \quad \leftarrow \text{arbitrary constant}$$

### Characteristics

1. Only defined for *reversible processes*; i.e., processes that are "quasi-static".
  - *Quasi-static process* = succession of equilibrium states.
  - *Equilibrium state* = state of system in which macroscopic properties (i.e., temp, volume, pressure, etc.) are constant.

2. Only defined for *equilibrium states*.

3. For infinitesimal changes in  $S_{\text{TD}}$ , can write

$$dS_{\text{TD}} = \delta Q_R / T$$

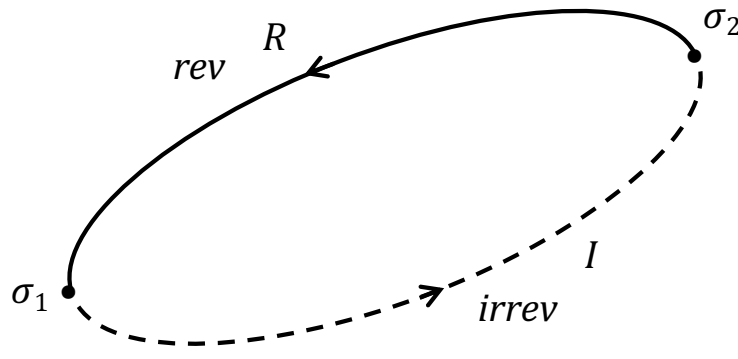
$1/T$  is an 'integrating factor' that converts a path-dependent function  $Q$  into a path-independent function  $S_{\text{TD}}$

For an *irreversible* process connecting equilibrium states  $\sigma_1$  and  $\sigma_2$ ,  $S_{\text{TD}}$  can still be calculated if there is, in principle, a reversible process that connects  $\sigma_1$  and  $\sigma_2$ .  
Ex: Heating a beaker of water.

- No reference to "disorder" or "chaos"!
- No reference to molecules or particles (gas or otherwise)!
- No reference to "information"!

### 3. Principle of Increasing $S_{\text{TD}}$

Consider an *irreversible* cycle:



Irreversible cycle consisting of an irreversible process  $I$  from  $\sigma_1$  to  $\sigma_2$ , followed by a reversible process  $R$  from  $\sigma_2$  back to  $\sigma_1$ .

- Clausius' inequality is 
$$\int_I^{\sigma_2} \frac{\delta Q}{T} + \int_R^{\sigma_1} \frac{\delta Q_R}{T} < 0 \quad \text{or} \quad \int_I^{\sigma_2} \frac{\delta Q}{T} - \int_R^{\sigma_1} \frac{\delta Q_R}{T} < 0$$

- Thus: 
$$\Delta S_{\text{TD}} = \int_R^{\sigma_2} \frac{\delta Q_R}{T} > \int_I^{\sigma_2} \frac{\delta Q}{T}$$
 ← Note: If the cycle was reversible (i.e., if the path  $I$  was reversible), then  $>$  would become  $=$ .

- So in general: 
$$\Delta S_{\text{TD}} = \int_R^{\sigma_2} \frac{\delta Q_R}{T} \geq \int_{\sigma_1}^{\sigma_2} \frac{\delta Q}{T}$$

- Now: Suppose the path from  $\sigma_1$  to  $\sigma_2$  is *thermally isolated*; i.e.,  $\delta Q = 0$ .

- Then: 

$\Delta S_{\text{TD}} \geq 0 \quad \text{or} \quad S_{\text{TD}}(\sigma_2) \geq S_{\text{TD}}(\sigma_1)$

The change in thermodynamic entropy for a thermally isolated irreversible process between equilibrium states increases, and is unaltered for a reversible process.

## 4. $S_{TD}$ and the Approach to Equilibrium

- How does the Principle of Increasing  $S_{TD}$  relate to the Equilibrium Principle?

  
One way of formulating the 2nd Law!

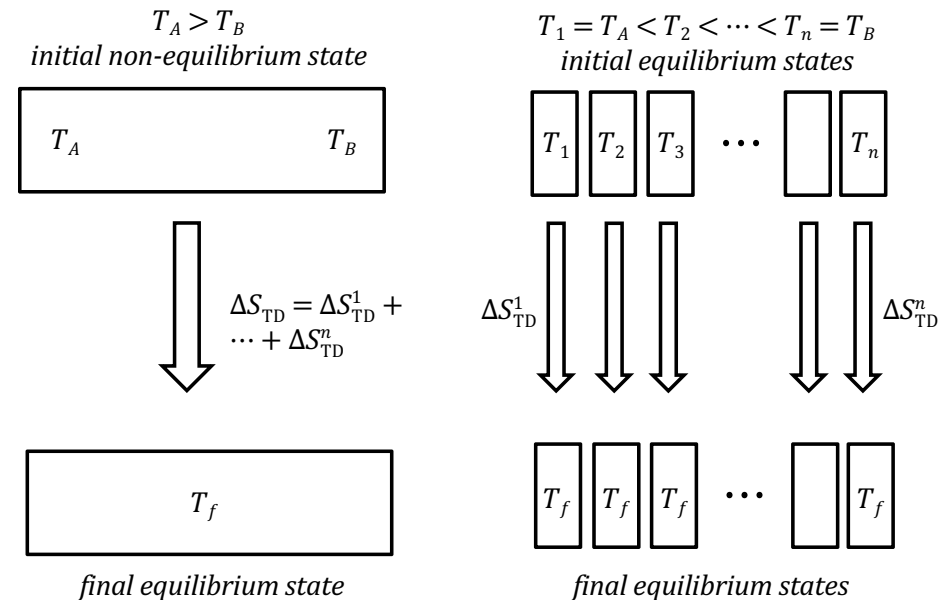
  
The Minus 1st Law!

- The "approach to equilibrium" is a process that connects a *non-equilibrium* state with an equilibrium state!

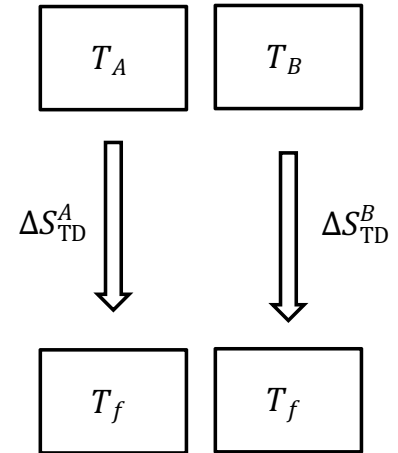
*How is  $S_{TD}$  defined for such a process? And does it increase/remains unaltered?*

### General method:

- System in initial *non-equilibrium* state can be decomposed into subsystems, each in an initial *equilibrium* state.
- Process that takes system from initial non-equilibrium state to final equilibrium state can be decomposed into a sum of processes that take each subsystem from its initial equilibrium state to final equilibrium state.
- Each sub-process has well-defined change in  $S_{TD}$ , and sum of these (i.e., change in  $S_{TD}$  for entire system) cannot be negative!



**Ex.** System composed of subsystems  $A, B$  with initial temps  $T_A, T_B$  and heat capacities  $C_A \equiv \delta Q_A/dT, C_B \equiv \delta Q_B/dT$  that are brought into contact and then allowed to reach equilibrium at temp  $T_f$ .



- System: initial *non-equilibrium* state  $\sigma_i$ , final *equilibrium* state  $\sigma_f$ .
- $A, B$ : initial *equilibrium* states  $\sigma_i^A, \sigma_i^B$ , final *equilibrium* states  $\sigma_f^A, \sigma_f^B$ .
- Suppose  $\sigma_i^A, \sigma_f^A$  are connected by a reversible process, at each step of which  $A$  absorbs a small amount of heat  $\delta Q_A = C_A dT$  from a reservoir resulting in an increase  $dT$  in temperature.
- Change in  $S_{TD}$  for  $A$  is:

$$\Delta S_{TD}^A = S_{TD}^A(\sigma_f^A) - S_A(\sigma_i^A) = \int_{\sigma_i^A}^{\sigma_f^A} \frac{\delta Q_A}{T} = \int_{T_A}^{T_f} \frac{C_A dT}{T} = C_A \ln \frac{T_f}{T_A}$$

Similarly for  $\Delta S_{TD}^B$

- Change in  $S_{TD}$  for entire system is:

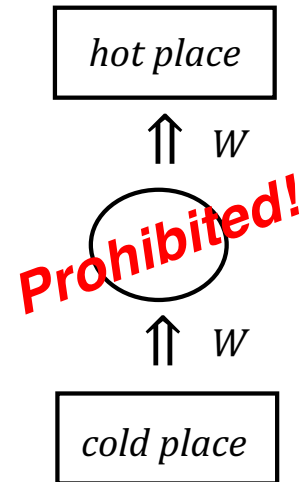
$$\Delta S_{TD}^A + \Delta S_{TD}^B = C_A \ln \frac{T_f}{T_A} + C_B \ln \frac{T_f}{T_B}$$

Claim: This expression cannot be negative!

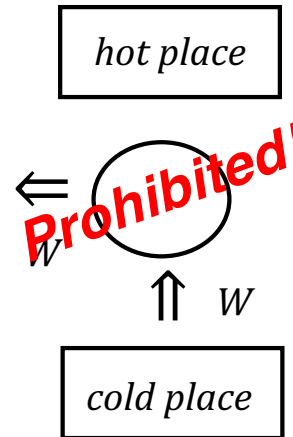
$$\begin{aligned} C_A \ln \frac{T_f}{T_A} + C_B \ln \frac{T_f}{T_B} &\geq C_A(1 - T_A/T_f) + C_B(1 - T_B/T_f) \quad \leftarrow \ln y \geq 1 - 1/y \\ &= T_f^{-1} [C_A(T_f - T_A) + C_B(T_f - T_B)] \\ &= T_f^{-1} (Q_A + Q_B) \\ &= 0 \quad \leftarrow \text{total work} = 0 \end{aligned}$$

## 5. Summary of 2nd Law of Thermodynamics

(1) Clausius Form: No cyclic process in which heat is transferred from cold to hot place without work input:



(2) Thomson Form: No cyclic process in which there is a conversion of heat to work without exhaust:



### Consequence of 2nd Law:

The *thermodynamic entropy*  $S_{TD}$  of a thermally isolated irreversible process between equilibrium states increases, and is unaltered for a reversible process.

*Absolute statements!*

*Meant to hold for any system subject to thermodynamical analysis.*

## Summary of Entailments

